

TLC374, TLC374Q, TLC374Y LinCMOS™ QUADRUPLE DIFFERENTIAL COMPARATORS

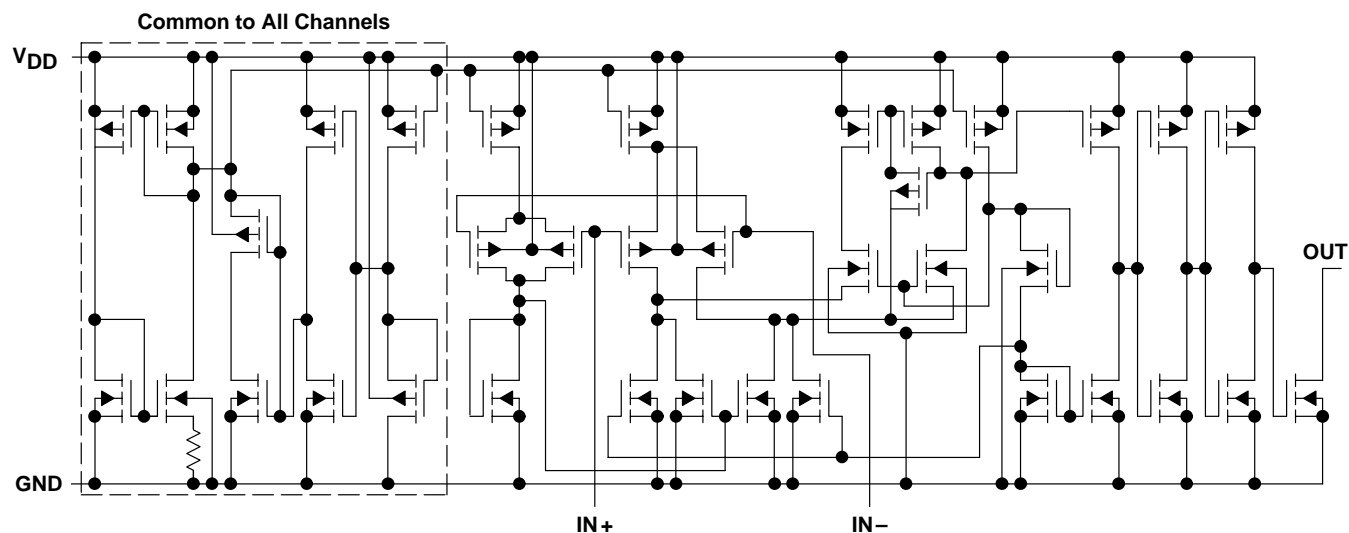
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AVAILABLE OPTIONS

T _A	V _{IO} max AT 25°C	PACKAGED DEVICES					CHIP FORM (Y)
		SMALL OUTLINE (D)	CHIP CARRIER (FK)	CERAMIC DIP (J)	PLASTIC DIP (N)	TSSOP (PW)	
0°C to 70°C	5 mV	TLC374CD	—	—	TLC374CN	TLC374CPW	TLC374Y
-40°C to 85°C	5 mV	TLC374ID	—	—	TLC374IN	—	—
-55°C to 125°C	5 mV	TLC374MD	TLC374MFK	TLC374MJ	TLC374MN	—	—
-40°C to 125°C	5 mV	TLC374QD	—	—	TLC374QN	—	—

The D packages are available taped and reeled. Add R suffix to device type (e.g., TLC374CDR).

equivalent schematic (each comparator)

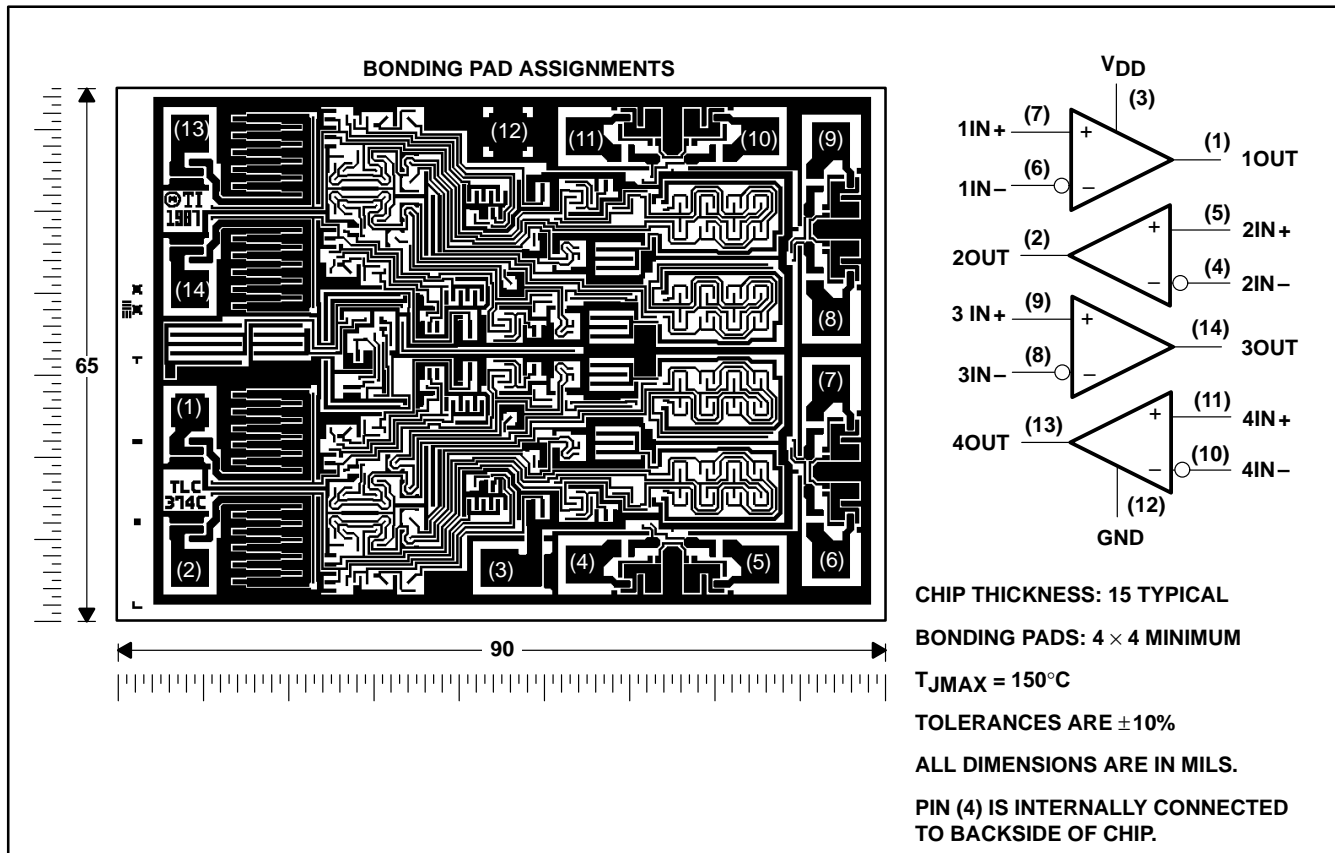


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TLC374Y chip information

This chip, when properly assembled, displays characteristics similar to the TLC374C. Thermal compression or ultrasonic bonding may be used on the doped-aluminum bonding pads. Chips may be mounted with conductive epoxy or a gold-silicon preform.



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absolute maximum ratings over operating free-air temperature range (unless otherwise noted)†

Supply voltage, V_{DD} (see Note 1)	18 V
Differential input voltage, V_{ID} (see Note 2)	± 18 V
Input voltage, V_I	V_{DD}
Input voltage range, V_I	-0.3 V to 18 V
Output voltage, V_O	18 V
Input current, I_I	± 5 mA
Output current, I_O	20 mA
Duration of output short circuit to ground (see Note 3)	unlimited
Continuous total power dissipation	See Dissipation Rating Table
Operating free-air temperature range, T_A : TLC374C	0°C to 70°C
TLC374I	-40°C to 85°C
TLC374M	-55°C to 125°C
TLC374Q	-40°C to 125°C
Storage temperature range, T_{stg}	-65°C to 150°C
Case temperature range for 60 seconds: FK package	260°C
Lead temperature 1,6 mm (1/16 inch) from case for 60 seconds: D, N, or PW package	260°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds: J package	300°C

† Stresses beyond those listed under “absolute maximum ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under “recommended operating conditions” is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

- NOTES: 1. All voltage values except differential voltages are with respect to network ground.
 2. Differential voltages are at $IN+$ with respect to $IN-$.
 3. Short circuits from outputs to V_{DD} can cause excessive heating and eventual device destruction.

DISSIPATION RATING TABLE

PACKAGE	$T_A \leq 25^\circ\text{C}$ POWER RATING	DERATING FACTOR	DERATE ABOVE T_A	$T_A = 70^\circ\text{C}$ POWER RATING	$T_A = 85^\circ\text{C}$ POWER RATING	$T_A = 125^\circ\text{C}$ POWER RATING
D	500 mW	7.6 mW/°C	84°C	500 mW	494 mW	190 mW
FK	500 mW	11.0 mW/°C	104°C	500 mW	500 mW	269 mW
J	500 mW	11.0 mW/°C	104°C	500 mW	500 mW	269 mW
N	500 mW	9.2 mW/°C	95°C	500 mW	500 mW	224 mW
PW	700 mW	5.6 mW/°C	—	448 mW	—	—

recommended operating conditions

	TLC374C		TLC374I		TLC374M		TLC374Q		UNIT
	MIN	MAX	MIN	MAX	MIN	MAX	MIN	MAX	
Supply voltage, V_{DD}	3	16	3	16	4	16	3	16	V
Common-mode input voltage, V_{IC}	$V_{DD} = 5$ V		0	3.5	0	3.5	0	3.5	V
	$V_{DD} = 10$ V		0	8.5	0	8.5	0	8.5	
Operating free-air temperature, T_A	0	70	-40	85	-55	125	-40	125	°C



electrical characteristics at specified free-air temperature, $V_{DD} = 5\text{ V}$

PARAMETER	TEST CONDITIONS	T_A †	TLC374C			TLC374I			TLC374M			UNIT	
			MIN	TYP	MAX	MIN	TYP	MAX	MIN	TYP	MAX		
V_{IO} Input offset voltage	$V_{IC} = V_{ICRmin}$, See Note 4	25°C		1	5		1	5		1	5	mV	
		Full range			6.5			7			10		
I_{IO} Input offset current		25°C		1			1			1		pA	
		MAX			0.3			1			10	nA	
I_{IB} Input bias current		25°C		5			5			5		pA	
		MAX			0.6			2			20	nA	
V_{ICR} Common-mode input voltage range		25°C	0 to $V_{DD}-1$			0 to $V_{DD}-1$			0 to $V_{DD}-1$			V	
		Full range	0 to $V_{DD}-1.5$			0 to $V_{DD}-1.5$			0 to $V_{DD}-1.5$				
I_{OH} High-level output current	$V_{ID} = 1\text{ V}$	$V_{OH} = 5\text{ V}$	25°C	0.1			0.1			0.1			nA
		$V_{OH} = 15\text{ V}$	Full range	1			1			1			μA
V_{OL} Low-level output voltage	$V_{ID} = -1\text{ V}$, $I_{OL} = 4\text{ mA}$	25°C		150	400		150	400		150	400	mV	
		Full range		700			700			700			
I_{OL} Low-level output current	$V_{ID} = -1\text{ V}$, $V_{OL} = 1.5\text{ V}$	25°C		6	16		6	16		6	16	mA	
I_{DD} Supply current (four comparators)	$V_{ID} = 1\text{ V}$, No load	25°C		300	600		300	600		300	600	mA	
		Full range		800			800			800			

† All characteristics are measured with zero common-mode input voltage unless otherwise noted. Full range is 0°C to 70°C for TLC374C, -40°C to 85°C for TLC374I, and -55°C to 125°C for the TLC374M, and -40°C to 125°C for TLC374Q. MAX is 70°C for TLC374C, 85°C TLC374I, and 125°C for the TLC374M, and 125°C for TLC374Q. IMPORTANT: See Parameter Measurement Information.

NOTE 4: The offset voltage limits given are the maximum values required to drive the output above 4 V or below 400 mV with a 10-k Ω resistor between the output and V_{DD} . They can be verified by applying the limit value to the input and checking for the appropriate output state.

switching characteristics, $V_{DD} = 5\text{ V}$, $T_A = 25^\circ\text{C}$

PARAMETER	TEST CONDITIONS	TLC374C, TLC374I TLC374M, TLC374Q			UNIT	
		MIN	TYP	MAX		
Response time	R_L connected to 5 V through 5.1 k Ω , $C_L = 15\text{ pF}$ ‡, See Note 5	100-mV input step with 5-mV overdrive			650	ns
		TTL-level input step			200	

‡ C_L includes probe and jig capacitance.

NOTE 5: The response time specified is the interval between the input step function and the instant when the output crosses 1.4 V.

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electrical characteristics at specified free-air temperature, $V_{DD} = 5\text{ V}$, $T_A = 25^\circ\text{C}$ (unless otherwise noted)

PARAMETER	TEST CONDITIONS	TLC374Y			UNIT
		MIN	TYP	MAX	
V_{IO} Input offset voltage	$V_{IC} = V_{ICRmin}$, See Note 4		1	5	mV
I_{IO} Input offset current			1		pA
I_{IB} Input bias current			5		pA
V_{ICR} Common-mode input voltage range		0 to $V_{DD}-1$			V
I_{OH} High-level output current	$V_{ID} = 1\text{ V}$, $V_{OH} = 5\text{ V}$		0.1		nA
V_{OL} Low-level output voltage	$V_{ID} = -1\text{ V}$, $I_{OL} = 4\text{ mA}$		150	400	mV
I_{OL} Low-level output current	$V_{ID} = -1\text{ V}$, $V_{OL} = 1.5\text{ mV}$	6	16		mA
I_{DD} Supply current (four comparators)	$V_{ID} = 1\text{ V}$, No load		300	600	μA

NOTE 4: The offset voltage limits given are the maximum values required to drive the output above 4 V or below 400 mV with a 10-k Ω resistor between the output and V_{DD} . They can be verified by applying the limit value to the input and checking for the appropriate output state.

switching characteristics, $V_{DD} = 5\text{ V}$, $T_A = 25^\circ\text{C}$

PARAMETER	TEST CONDITIONS		TLC374Y			UNIT
			MIN	TYP	MAX	
Response time	R_L connected to 5 V through 5.1 k Ω , $C_L = 15\text{ pF}$ †, See Note 5	100-mV input step with 5-mV overdrive		650		ns
		TTL-level input step		200		

† C_L includes probe and jig capacitance.

NOTE 4: The response time specified is the interval between the input step function and the instant when the output crosses 1.4 V.



PARAMETER MEASUREMENT INFORMATION

The digital output stage of the TLC374 can be damaged if it is held in the linear region of the transfer curve. Conventional operational amplifier/comparator testing incorporates the use of a servo loop that is designed to force the device output to a level within this linear region. Since the servo-loop method of testing cannot be used, the following alternative for measuring parameters such as input offset voltage, common-mode rejection, etc., are offered.

To verify that the input offset voltage falls within the limits specified, the limit value is applied to the input as shown in Figure 1(a). With the noninverting input positive with respect to the inverting input, the output should be high. With the input polarity reversed, the output should be low.

A similar test can be made to verify the input offset voltage at the common-mode extremes. The supply voltages can be slewed as shown in Figure 1(b) for the V_{ICR} test, rather than changing the input voltages, to provide greater accuracy.

A close approximation of the input offset voltage can be obtained by using a binary search method to vary the differential input voltage while monitoring the output state. When the applied input voltage differential is equal, but opposite in polarity to the input offset voltage, the output changes state.

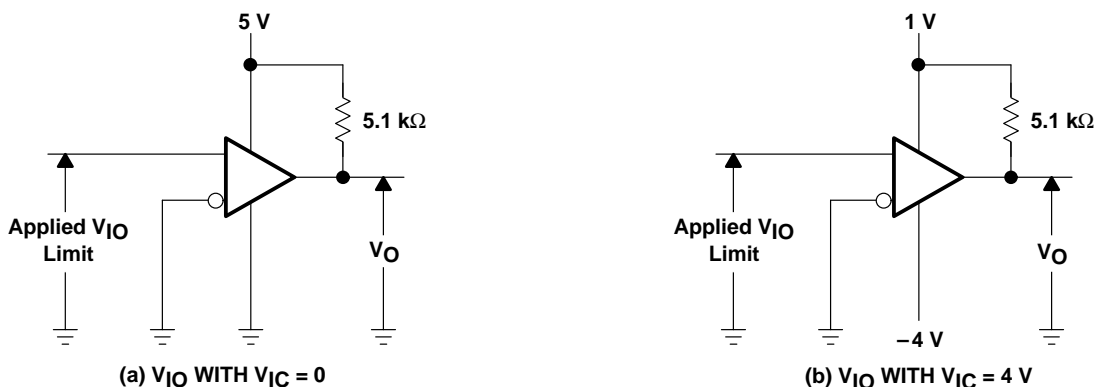


Figure 1. Method for Verifying That Input Offset Voltage is Within Specified Limits

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PARAMETER MEASUREMENT INFORMATION

Figure 2 illustrates a practical circuit for direct dc measurement of input offset voltage that does not bias the comparator into the linear region. The circuit consists of a switching-mode servo loop in which U1a generates a triangular waveform of approximately 20-mV amplitude. U1b acts as a buffer with C2 and R4 removing any residual dc offset. The signal is then applied to the inverting input of the comparator under test, while the noninverting input is driven by the output of the integrator formed by U1c through the voltage divider formed by R9 and R10. The loop reaches a stable operating point when the output of the comparator under test has a duty cycle of exactly 50%, which can only occur when the incoming triangle wave is sliced symmetrically or when the voltage at the noninverting input exactly equals the input offset voltage.

Voltage divider R9 and R10 provide a step up of the input offset voltage by a factor of 100 to make measurement easier. The values of R5, R8, R9, and R10 can significantly influence the accuracy of the reading; therefore, it is suggested that their tolerance level be 1% or lower.

Measuring the extremely low values of input current requires isolation from all other sources of leakage current and compensation for the leakage of the test socket and board. With a good picoammeter, the socket and board leakage can be measured with no device in the socket. Subsequently, this open-socket leakage value can be subtracted from the measurement obtained with a device in the socket to obtain the actual input current of the device.

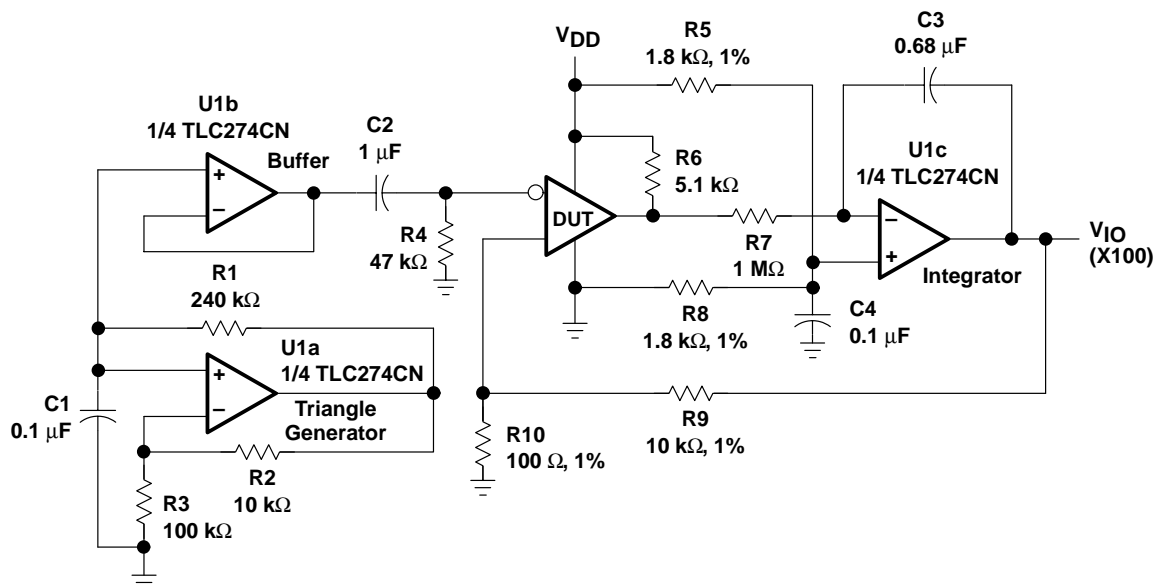
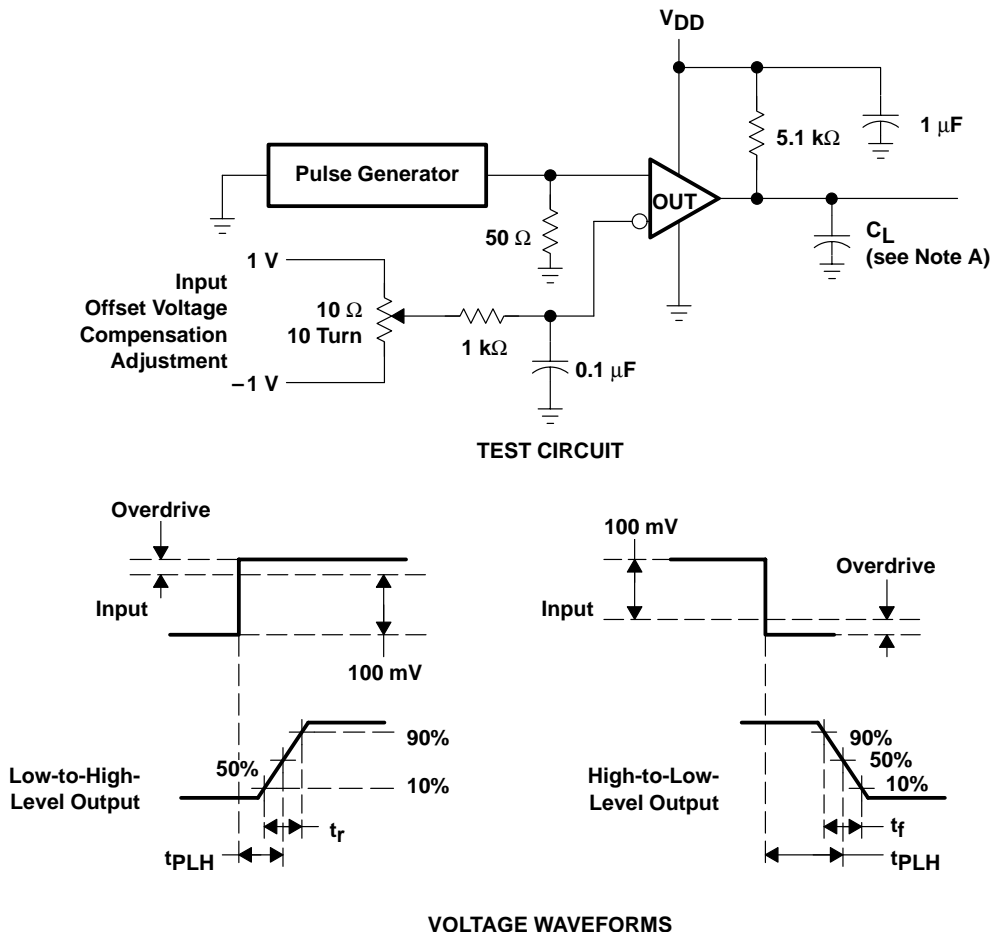


Figure 2. Test Circuit for Input Offset Voltage Measurement

PARAMETER MEASUREMENT INFORMATION

Response time is defined as the interval between the application of an input step function and the instant when the output reaches 50% of its maximum value. Response time, low-to-high-level output, is measured from the trailing edge of the input pulse. Response-time measurement at low input signal levels can be greatly affected by the input offset voltage. The offset voltage should be balanced by the adjustment at the inverting input (as shown in Figure 3) so that the circuit is just at the transition point. Then a low signal, for example, 105-mV or 5-mV overdrive, causes the output to change state.



NOTE A: C_L includes probe and jig capacitance.

Figure 3. Response, Rise, and Fall Times Test Circuit and Voltage Waveforms

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PRINCIPLES OF OPERATION

LinCMOS process

LinCMOS process is a linear polysilicon-gate complimentary-MOS process. Primarily designed for single-supply applications, LinCMOS products facilitate the design of a wide range of high-performance analog functions from operational amplifiers to complex mixed-mode converters.

While digital designers are experienced with CMOS, MOS technologies are relatively new for analog designers. This short guide is intended to answer the most frequently asked questions related to the quality and reliability of LinCMOS products. Further questions should be directed to the nearest TI field sales office.

electrostatic discharge

CMOS circuits are prone to gate oxide breakdown when exposed to high voltages even if the exposure is only for very short periods of time. Electrostatic discharge (ESD) is one of the most common causes of damage to CMOS devices. It can occur when a device is handled without proper consideration for environmental electrostatic charges, e.g. during board assembly. If a circuit in which one amplifier from a dual operational amplifier is being used and the unused pins are left open, high voltages tends to develop. If there is no provision for ESD protection, these voltages may eventually punch through the gate oxide and cause the device to fail. To prevent voltage build up, each pin is protected by internal circuitry.

Standard ESD-protection circuits safely shunt the ESD current by providing a mechanism whereby one or more transistors break down at voltages higher than normal operating voltages but lower than the breakdown voltage of the input gate. This type of protection scheme is limited by leakage currents which flow through the shunting transistors during normal operation after an ESD voltage has occurred. Although these currents are small, on the order of tens of nanoamps, CMOS amplifiers are often specified to draw input currents as low as tens of picoamps.

To overcome this limitation, TI design engineers developed the patented ESD-protection circuit shown in Figure 4. This circuit can withstand several successive 2-kV ESD pulses, while reducing or eliminating leakage currents that may be drawn through the input pins. A more detailed discussion of the operation of TI's ESD-protection circuit is presented on the next page.

All input an output pins of LinCMOS and Advanced LinCMOS products have associated ESD-protection circuitry that undergoes qualification testing to withstand 2000 V discharged from a 100-pF capacitor through a 1500-Ω resistor (human body model) and 200 V from a 100-pF capacitor with no current-limiting resistor (charged device model). These tests simulate both operator and machine handling of devices during normal test and assembly operations.

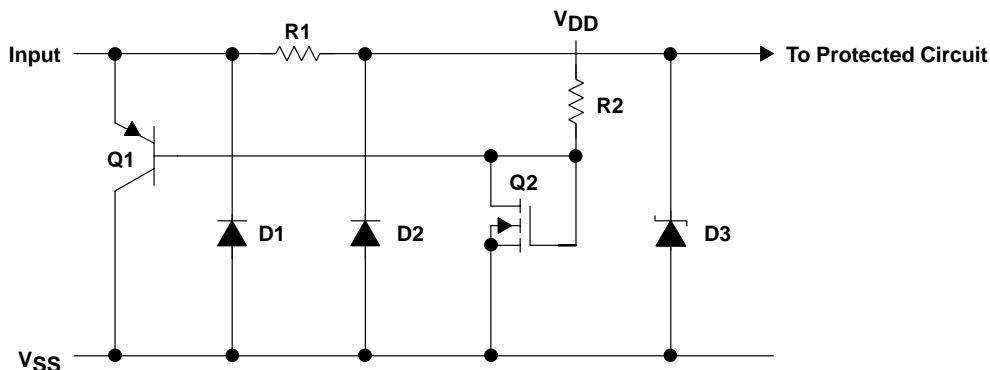


Figure 4. LinCMOS ESD-Protection Schematic

PRINCIPLES OF OPERATION

Input protection circuit operation

Texas Instruments patented protection circuitry allows for both positive- and negative-going ESD transients. These transients are characterized by extremely fast rise times and usually low energies, and can occur both when the device has all pins open and when it is installed in a circuit.

positive ESD transients

Initial positive charged energy is shunted through Q1 to V_{SS} . Q1 turns on when the voltage at the input rises above the voltage on V_{DD} by a value equal to the V_{BE} of Q1. The base current increases through R2 with input current as Q1 saturates. The base current through R2 as Q1 saturates forces the voltage at the drain and gate of Q2 to exceed its threshold level ($V_T \sim 22$ to 26 V) and turn on Q2. The shunted input current through Q1 to V_{SS} is now shunted through the n-channel enhancement-type MOSFET Q2 to V_{SS} . If the voltage on the input pin continues to rise, the breakdown voltage of D3 is exceeded and all remaining energy is dissipated in R1 and D3. The breakdown voltage of D3 is designed to be 24 V to 27 V, which is well below the gate oxide voltage of the circuit to be protected.

negative ESD transients

The negative charged ESD transients are shunted directly through D1. Additional energy is dissipated in R1 and D2 as D2 becomes forward-biased. The voltage seen by the protected circuit is -0.3 V to -1 V (the forward voltage of D1 and D2).

circuit-design considerations

LinCMOS products are being used in actual circuits environments that have input voltages that exceed the recommended common-mode input voltage range and activate the input protection circuit. Even under normal operation, these conditions occur during circuit power up or power down, and in many cases, when the device is being used for a signal conditioning function. The input voltages can exceed V_{ICR} and not damage the device only if the inputs are current limited. The recommended current limit shown on most product data sheets is ± 5 mA. Figures 5 and 6 show typical characteristics for input voltage vs input current.

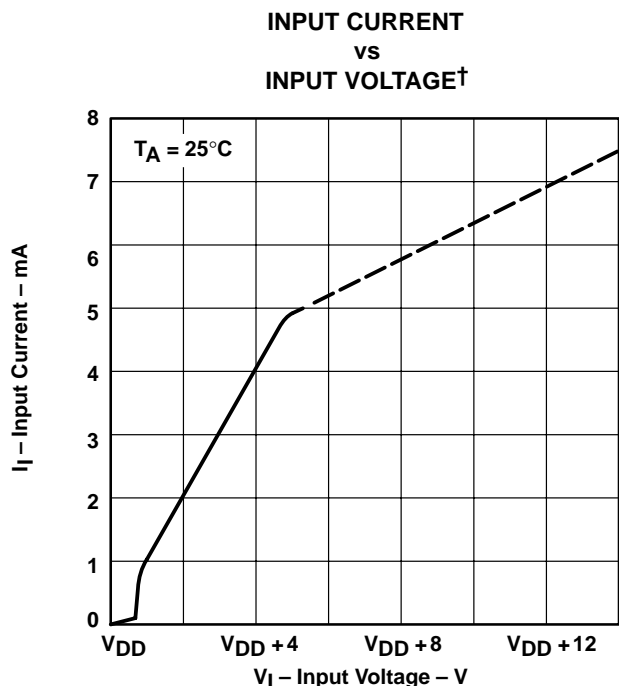
Normal operation and correct output state can be expected even when the input voltage exceeds the positive supply voltage. The input current should be externally limited even though internal positive current limiting is achieved in the input protection circuit by the action of Q1. When Q1 is on, it saturates and limit the current to approximately 5-mA collector current by design. When saturated, Q1 base current increases with input current. This current is forced into the V_{DD} pin and into the device I_{DD} or the V_{DD} supply through R2 producing the current limiting effects shown in Figure 5. This internal limiting lasts only as long as the input voltage is below the V_T of Q2.

When the input voltage exceeds the negative supply voltage, normal operation is affected and output voltage states may not be correct. Also, the isolation between channels of multiple devices (duals and quads) can be severely affected. External current limiting must be used since this current is directly shunted by D1 and D2, and no internal limiting is achieved. If normal output voltage states are required, an external input voltage clamp is required (see Figure 7).

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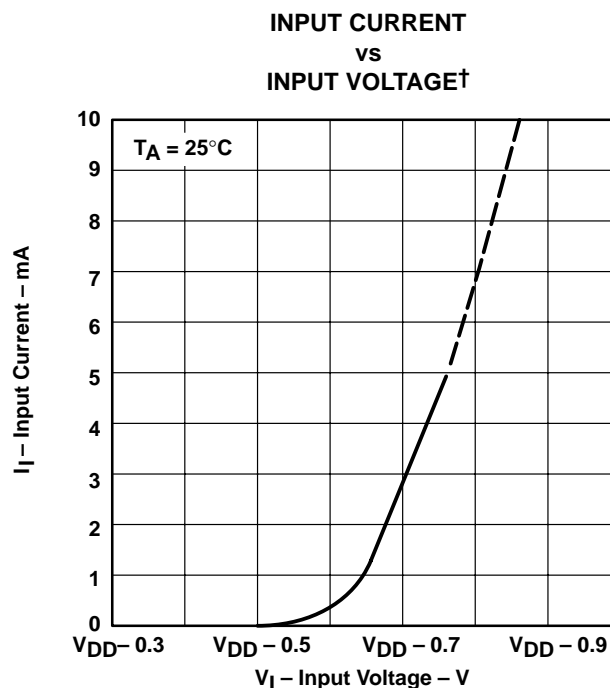
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PRINCIPLES OF OPERATION



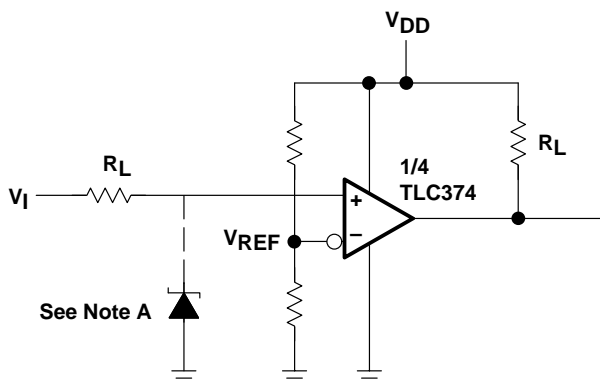
† The dashed line identifies an area of operation where some degradation of parametric performance may be experienced.

Figure 5



† The dashed line identifies an area of operation where some degradation of parametric performance may be experienced.

Figure 6



Positive Voltage Input Current Limit:

$$R_I = \frac{+V_I - V_{DD} - 0.3 \text{ V}}{5 \text{ mA}}$$

Negative Voltage Input Current Limit:

$$R_I = \frac{-V_I - V_{DD} - (0.3 \text{ V})}{5 \text{ mA}}$$

NOTE A: If the correct output state is required when the negative input exceeds V_{SS} , a Schottky clamp is required.

Figure 7. Typical Input Current-Limiting Configuration for a LinCMOS Comparator

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