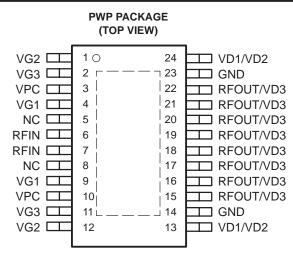
SLWS059B - MAY 1997 - REVISED AUGUST 1998

- Single Positive Power Supply (No Negative Voltage Required)
- Advanced Silicon RFMOS<sup>™</sup> Technology
- 4.8-V Operation for GSM Applications
- 35-dBm Typical Output Power
- 30-dB Typical Power Gain
- 40% Typical PAE with 5-dBm Input Power
- 45% Typical PAE with 8-dBm Input Power
- Output Power Control
- Few External Components Required for Operation
- Thermally Enhanced Surface-Mount Package for Small Circuit Footprint
- Rugged, Sustains 20:1 Load Mismatch
- 800-MHz to 1000-MHz Wide Operational Frequency Range
- Low Standby Current (<10 μA)

#### description



NC – No internal connection

The TRF7610 is a silicon MOSFET power amplifier IC for 900-MHz applications, tailored specifically for global systems for mobile communications (GSM). It uses Texas Instruments RFMOS<sup>™</sup> process and consists of a three-stage amplifier with output power control. Few external components are required for operation.

The TRF7610 amplifies the RF signal from a preceding modulator and the upconverter stages in an RF section of a transmitter to a level that is sufficient for connection to the antenna. The RF input port, RFIN, and the RF output port, RFOUT, require simple external matching networks.

A control signal applied to the VPC input can ramp the RF output power up or down to meet ramp and spurious emission specifications for time-division multiple-access (TDMA) systems. The power control signal causes a change in output power as the voltage applied to VPC varies between 0 V and 3 V. With the RF input power applied to RFIN at 5 dBm, adjusting VPC from 0 V to 3 V increases the output power from a typical value of -43 dBm at VPC = 0 V to a typical value of 35 dBm at VPC = 3 V. Forward isolation with the RF input power applied to RFIN at 5 dBm, VPC = 0 V, is typically 48 dB.

The TRF7610 is available in a thermally enhanced, surface-mount, 24-pin PowerPAD<sup>™</sup> (PWP) thin-shrink small-outline package (TSSOP). It is characterized for operation from -40°C to 85°C operating free-air temperature. In order to maintain acceptable thermal operating conditions, the device should be operated in pulse applications such as the GSM standard 1/8 duty cycle. The package has a solderable pad that improves the package thermal performance by bonding the pad to an external thermal plane. The pad also acts as a low-inductance electrical path to ground and must be electrically connected to the printed circuit-board (PCB) ground plane as a continuation of the regular package terminals that are designated GND.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.



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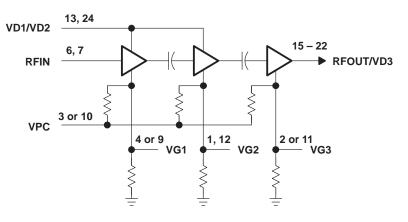
PRODUCTION DATA information is current as of publication date. Products conform to specifications per the terms of Texas Instruments standard warranty. Production processing does not necessarily include testing of all parameters.



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SLWS059B - MAY 1997 - REVISED AUGUST 1998

### schematic



## **Terminal Functions**

TERMINAL			DESCRIPTION		
NAME	NO.	1/0	DESCRIPTION		
GND	14, 23		Analog ground for all internal circuits. All signals are referenced to the ground terminals.		
NC	5, 8		No internal connection. It is recommended that all NC terminals be connected to ground.		
RFIN	6, 7	I	RF input. RFIN accepts signals between 800 MHz and 1000 MHz.		
RFOUT/VD3	15, 16, 17, 18, 19, 20, 21, 22	I/O	RF output and third-stage drain bias. RFOUT requires an external matching network.		
VG1	4, 9	1	First-stage gate bias set by resistor. Either terminal may be used or both may be connected externally.		
VG2	1, 12	1	Second-stage gate bias set by resistor. These terminals must be connected externally.		
VG3	2, 11	1	Third-stage gate bias set by resistor. Either terminal may be used or both may be connected externally.		
VPC	3, 10	1	Voltage power control. VPC is a signal between 0 V and 3 V that adjusts the output power from a typical value of $-43$ dBm to 35 dBm. Either terminal may be used, or both may be connected externally.		
VD1/VD2	13, 24	I	First- and second-stage drain bias. These terminals must be connected externally.		

## absolute maximum ratings over operating free-air temperature range (unless otherwise noted)<sup>†</sup>

Supply voltage range, V <sub>DD</sub> (see Note 1)	–0.6 V to 8 V
Input voltage range, VPC	$\ldots \ldots -0.6$ V to 4 V
Input power at RFIN	13 dBm
Thermal resistance, junction to case, R <sub>θ,JC</sub> (see Note 2)	3.5°C/W
Junction temperature, Tjmax	150°C
Operating free-air temperature range, T <sub>A</sub>	40°C to 85°C
Storage temperature range, T <sub>stg</sub>	–65°C to 150°C

<sup>†</sup> Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

NOTES: 1. Voltage values are with respect to GND.

2. No air flow and with infinite heatsink



## recommended operating conditions

PARAMETER	MIN	NOM	MAX	UNIT
Supply voltage V <sub>DD</sub> (see Note 1 and Note 3)	3.5	4.8	6	V
Operating free-air temperature, T <sub>A</sub>	-40		85	°C
Operating frequency range (see Note 4)			1000	MHz

NOTES: 1. Voltage values are with respect to GND.

3 .Performance varies with drain voltage, see Figure 8.

4. External matching network dependent.

### electrical characteristics over full range of recommended operating conditions

### supply current, $V_{DD}$ = 4.8 V

	PARAMETER	TEST CONDITIONS	ΜΙΝ ΤΥΡ <sup>†</sup> ΜΑΧ	UNIT		
In a Cumply symposit	Operating at maximum output power	VPC = 3 V	2	A		
IDD Supply current	Operating with no RF input power	VPC = 0 V	<10	μA		

<sup>†</sup> Typical values are at  $T_A = 25^{\circ}C$ 

## GSM operation, $V_{DD}$ = 4.8 V, VPC = 3 V, P<sub>I</sub> = 5 dBm, T<sub>A</sub> = 25°C (unless otherwise noted)<sup>‡</sup>

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
Operating frequency range		870		925	MHz		
Output power		VPC = 3 V	34	35	36	dBm	
		VPC = 0 V		-43			
Dower added officiancy (DAE)		40%					
Power added efficiency (PAE)		PI = 8 dBm		45%			
Input return loss (externally matched, s	P <sub>I</sub> = -20 dBm	10		dB			
	2f <sub>0</sub>	With external matching	-28		dBc		
Harmonics	3f <sub>0</sub>	With external matching	-40				
	20 MHz above f <sub>0</sub>			-88		JD	
Noise power in 30-kHz bandwidth	10 MHz above f <sub>0</sub>		-88		dBm		
Ruggedness test		Frequency = 900 MHz, Load VSWR = 20:1, All phase angles		§			

<sup>‡</sup> Specific applications circuit

§ No degradation in output power after test.

### stability, GSM operation

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
	Output VSWR¶ < 6:1 all phases, $V_{DD}$ < 6 V, PJ = 5 dBm, $P_O \le 35$ dBm, Output frequency band: 200 MHz – 1200 MHz		parasiti llations ( ıs < –70	(all	

VSWR = voltage standing wave ratio

### switching characteristics

### **GSM** operation

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
ton	Switching time, RF output OFF to ON	VPC stepped from 0 V to 3 V		2		μs
toff	Switching time, RF output ON to OFF	VPC stepped from 3 V to 0 V		2		μs



SLWS059B - MAY 1997 - REVISED AUGUST 1998

## **APPLICATION INFORMATION**

In all cases, a capacitor must be connected from the positive power supply to ground as close to the terminals as possible for power-supply bypassing. The dc-blocking capacitors are required on the RF input and RF output. A list of components and their functions is shown in Table 1.

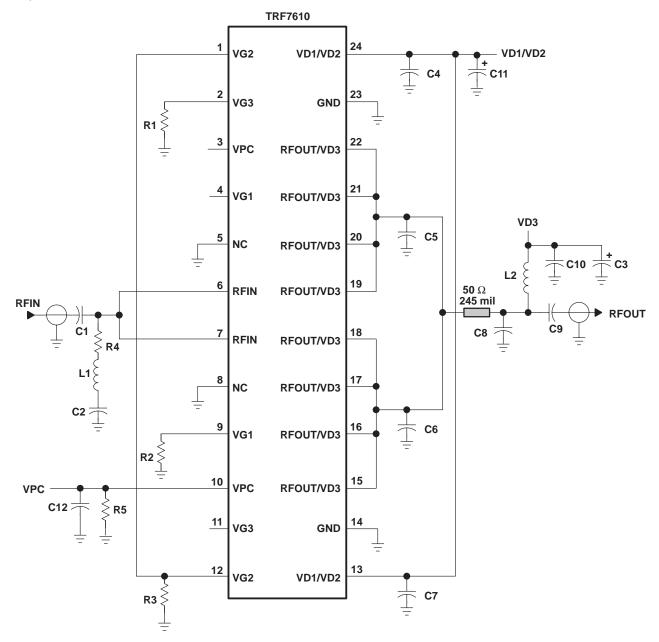


Figure 1. Typical GSM Cellular Telephone Application



COMPONENT DESIGNATION	TYPICAL VALUE	FUNCTION			
C1	100 pF	DC blocking capacitor			
C2	100 pF	Matching capacitor			
C3	330 μF	Drain-bias decoupling capacitor			
C4	0.033 μF	Drain-bias decoupling capacitor			
C5, C6	22 pF	High-Q matching capacitor			
C7	0.033 μF	Drain-bias decoupling capacitor			
C8	11 pF	High-Q matching capacitor			
C9	100 pF	DC blocking capacitor			
C10	100 pF	Drain-bias decoupling capacitor			
C11	100 μF	Drain-bias decoupling capacitor			
C12	100 pF	Decoupling capacitor			
R1	2200 Ω	Gate-bias setting resistor			
R2, R3	5100 Ω	Gate-bias setting resistor			
R4	3.9 Ω	Matching resistor			
R5	51 Ω	Vpc termination resistor			
L1	2.7 nH	Matching inductor			
L2	18.5 nH high-current inductor or $\lambda/4$ microstrip line <sup>†</sup>	Drain bias inductor			

**Table 1. External Component Selection** 

<sup>†</sup>On a FR4 substrate with  $\in_{\Gamma}$  of 4.3, a  $\lambda/4$  50  $\Omega$  line is 40 mm.

### design philosophy

The TRF7610 is a three-stage integrated power amplifier for use in cellular phone handsets. The device and applications board are optimized to operate under 900-MHz, 4.8-V GSM conditions. External matching networks provide design flexibility in centering the frequency response from 800 to 1000 MHz. Typical performance at 900 MHz, driven by a 5-dBm GSM signal, is 30 dB of power gain, 35 dBm output power, and 40 percent PAE.

Discrete component selection was made to optimize output power, gain, pulse flatness in the GSM pulse window, and PAE. Where possible, size and cost goals were considered: the smallest, least expensive components available were included in the applications board design. Some of the components, however, were chosen for their ability to increase performance. The following sections explain the design options and compromises to consider when substituting parts of differents types and values.

### output matching network

The output matching network provides the majority of the design flexibility. First, the shunt capacitors, C5, C6, and C8 are American Technical Ceramics high-Q capacitors, which increase performance. The ATC capacitors achieve a 0.4-dB increase in output power and a 3-percent increase in PAE compared to the performance achieved using 0402-sized capacitors. However, if size and cost are more important, 0402-sized capacitors can be used, while sacrificing the performance gains achieved using the high-Q capacitors.

Second, the dc bias network on the amplifier output stage, designed using a Coilcraft 18.5 nH high-current inductor (L2), minimizes the board layout area. An alternative to this high-current inductor is a quarter-wave stub with a bias decoupling capacitor to ground (C10, C3). On the FR4 board with  $\epsilon_r = 4.3$ , a quarter-wave stub at 900 MHz is 40 mm in length. One advantage that the quarter-wave stub offers over the inductor is improved second harmonic suppression. The inductor offers a much smaller footprint; however, it does sacrifice 10 dB



of second harmonic suppression. The PAE is only slightly affected: it is reduced by approximately 1 percent compared to the quarter-wave stub. The system designer must decide if size or performance is of greatest concern.

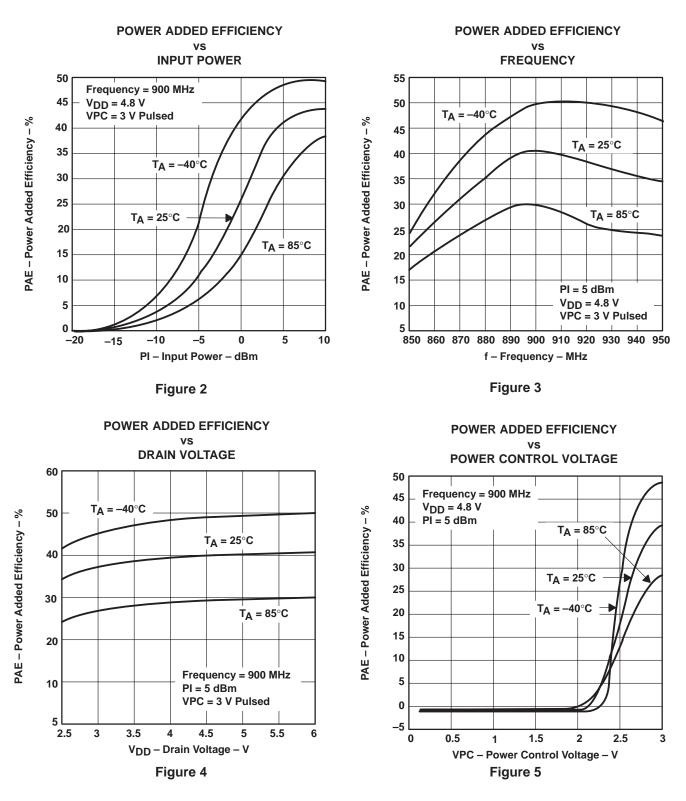
The 330  $\mu$ F bias decoupling capacitors, C3 and C11, provide pulse flatness in the GSM application. These surface mount capacitors provide a gain slope of -0.4 dB over the duration of the GSM duty cycle. If that is not acceptable, the performance can be improved by adding a larger value capacitor in parallel with the two existing capacitors. Measured results, using a standard 4700  $\mu$ F electrolytic taken from a cellular phone, is -0.1 dB of gain slope for the duration of the GSM duty cycle. Capacitor size considerations must be decided by the system designer.

### dc bias network

The dc bias network consists of resistors R1, R2, R3, and R5, which set the gate bias voltage of the device. R1, R2, and R3 are used as voltage divider resistors which set the gate voltages at approximately 1.7 V. Resistor R5 is a 51  $\Omega$  termination resistor that is needed only for a 50  $\Omega$  pulse generator. When a high-impedance pulse generator is used, the 51  $\Omega$  resistor can be omitted as it is not necessary for device function.

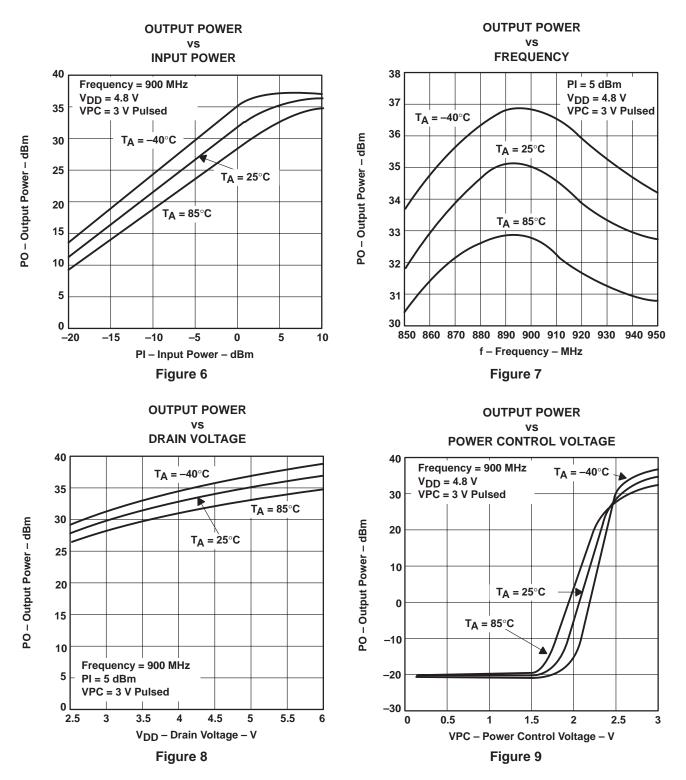








SLWS059B - MAY 1997 - REVISED AUGUST 1998







## **TYPICAL CHARACTERISTICS**

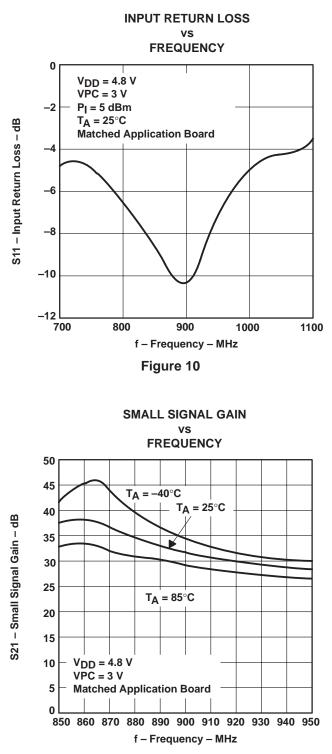


Figure 11

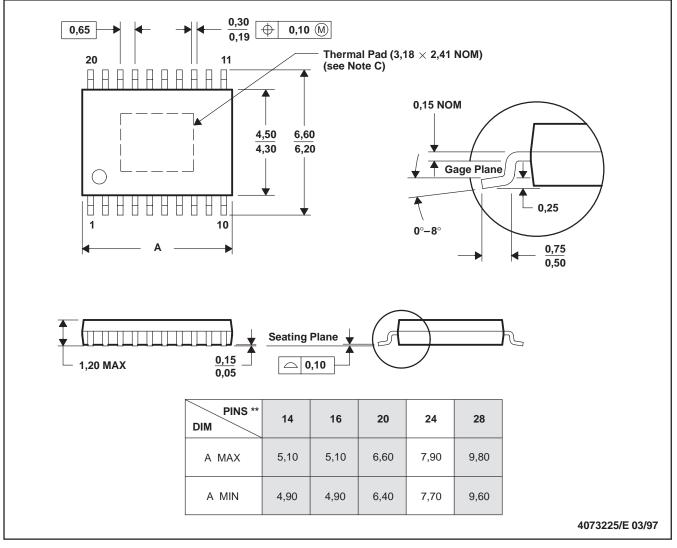


SLWS059B - MAY 1997 - REVISED AUGUST 1998

MECHANICAL DATA

### PWP (R-PDSO-G\*\*)

### PowerPAD<sup>™</sup> PLASTIC SMALL-OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.

B. This drawing is subject to change without notice.

C. The package thermal performance may be enhanced by bonding the thermal pad to an external thermal plane. This solderable pad is electrically and thermally connected to the backside of the die.



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