

Audio preamplifiers LM381, HA12017 and 6270

Stock numbers 306-825, 304-576, 302-132

Two high quality audio preamplifier i.c.s. suitable for magnetic cartridge amplification using RIAA equalisation, or microphone amplification using a "flat" characteristic. Also a microphone preamplifier incorporating a Voice Operated Gain Adjusting Device (V.O.G.A.D.).

LM381

A dual preamplifier specially designed to meet the requirements of amplifying low level signals in low noise applications. Each amplifier contains an internal power supply decoupler-regulator, providing 120dB supply rejection and 60dB channel separation. Other features include high gain, large output voltage swing and a wide power bandwidth. Operation is from a single supply in the range 9 to 40V and the device is internally compensated and short-circuit protected.

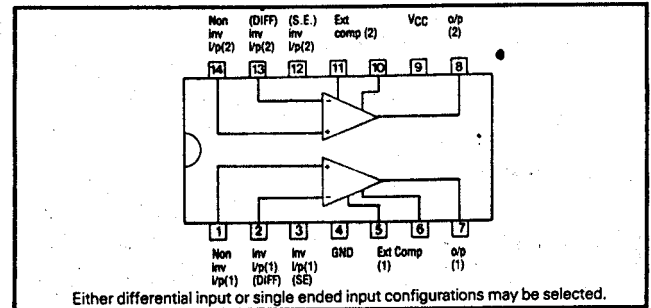
Maximum ratings

Supply voltage _____ 40V
 Dissipation _____ 715mW
 Operating temperature range _____ 0 to 70°C
 Input voltage for linear swing _____ 300mV rms

Applications

Typical electrical characteristics

Voltage gain open loop single ended _____ 320,000 (110dB)
 Voltage gain open loop single differential _____ 160,000 (104dB)
 Total supply current ($R_L = \infty$) _____ 10mA
 Input resistance _____ 100k Ω
 Open loop output resistance _____ 150 Ω
 Voltage swing _____ $V_{CC} - 2V$
 Full power bandwidth _____ 75kHz
 Channel separation _____ 60dB
 Harmonic distortion at 60dB gain _____ 0.1% at 1kHz



NOTES
 A ready made pc board RS stock number 434-396 is available to accommodate the LM381 and associated components (including the tone and volume controls) for a stereo pre-amplifier giving RIAA flat characteristics.

Figure 1 Magnetic cartridge amplifier to the RIAA characteristic

An amplifier to RIAA characteristics for use with dynamic cartridges with a standard load of 50k Ω . When a crystal or ceramic cartridge is used the LM381 "single ended amplifier" circuit may be connected directly. Gain $\approx \frac{30,000}{R_e \Omega}$

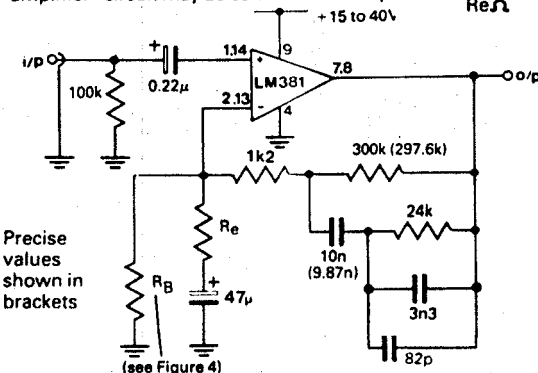
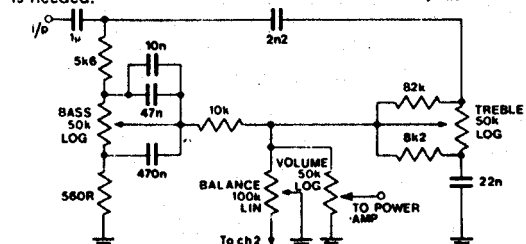
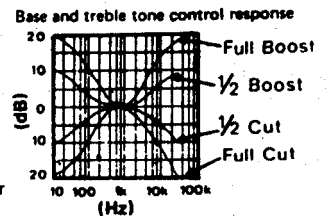


Figure 2 Tone control stage

Some audio applications require bass and treble tone controls. Normally two preamplifiers are required to compensate for the insertion loss of the controls. However, due to the excellent gain and large output of the LM381, only a single preamplifier is needed.



The i/p of the tone control stage can be put in series with any preamplifier circuit.

Figure 3 Audio mixer

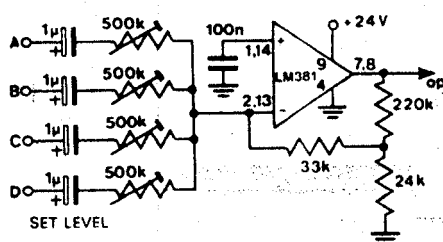


Figure 4 Biasing

For supply voltages other than those shown use the formula below to determine the correct biasing point.

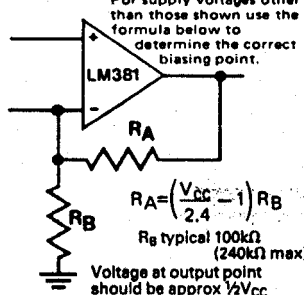


Figure 5 Biasing - split supply

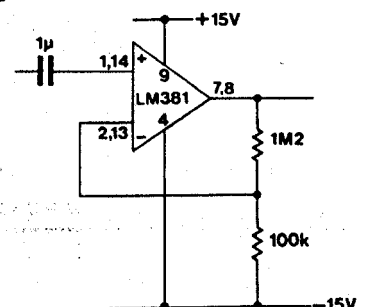
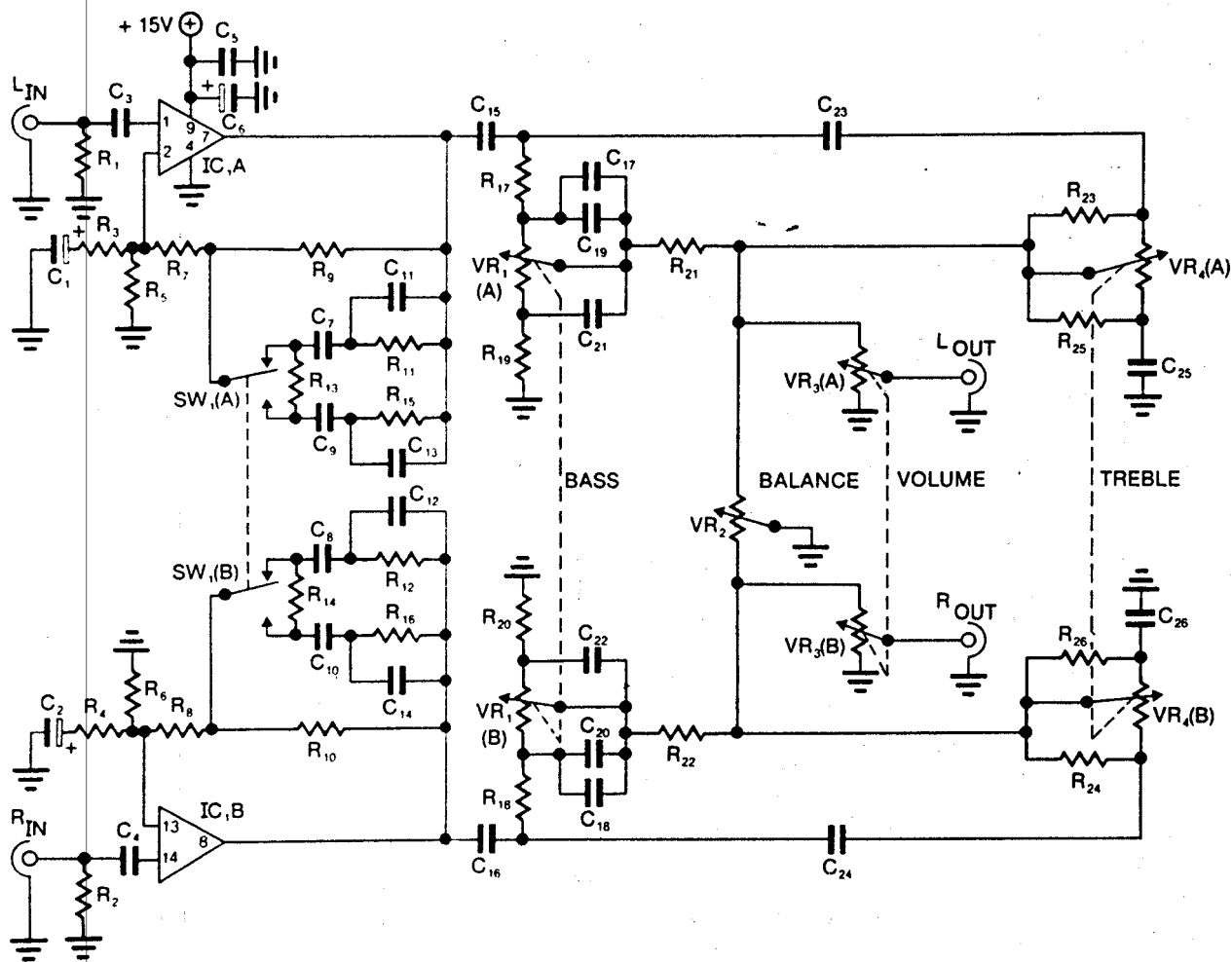


Figure 6 Circuit diagram of preamplifier using RS printed circuit board 434-396



List of components

Resistors

| | | |
|---|------|---------|
| R ₁ R ₂ R ₁₁ R ₁₂ | 47k | 148-893 |
| R ₃ R ₄ | 120R | 148-281 |
| R ₅ R ₆ | 100k | 148-972 |
| R ₇ R ₈ | 1k2 | 148-528 |
| R ₉ R ₁₀ | 510k | 149-155 |
| R ₁₃ R ₁₄ | 10M | 158-159 |
| R ₁₅ R ₁₆ | 750R | 148-477 |
| R ₁₇ R ₁₈ | 5k6 | 148-679 |
| R ₁₉ R ₂₀ | 560R | 148-449 |
| R ₂₁ R ₂₂ | 10k | 148-736 |
| R ₂₃ R ₂₄ | 82k | 148-950 |
| R ₂₅ R ₂₆ | 8k2 | 148-714 |

All 0.25W Metal Film except R₁₃ R₁₄ Hi-Stab Carbon Film.

Miscellaneous

| | | |
|---|----------|---------|
| VR ₁ VR ₃ VR ₄ | 50k Log | 162-451 |
| VR ₂ | 100k Lin | 161-818 |
| IC ₁ | LM 381 | 306-825 |
| SW ₁ | D.P.D.T. | 327-658 |
| IC socket | 14-pin | 402-305 |
| P.C.B. | | 434-396 |

Capacitors

| | | | |
|---------------------------------|------|-------------------------|---------|
| C ₁ C ₂ | 47μ | 16V P.C.B. Electrolytic | 104-461 |
| C ₃ C ₄ | 100n | 63V Polyester | 114-840 |
| C ₅ | 100n | 30V Disc Ceramic | 124-178 |
| C ₆ | 470μ | 16V P.C.B. Electrolytic | 104-499 |
| C ₇ C ₈ | 6n8 | 160V Polystyrene | 113-386 |
| C ₉ C ₁₀ | 2μ2 | 100V Polyester | 114-446 |
| C ₁₁ C ₁₂ | 1n5 | 160V Polystyrene | 113-336 |
| C ₁₃ C ₁₄ | 33p | 160V Polystyrene | 113-235 |
| C ₁₅ C ₁₆ | 1μ | Min. Dipped Polyester | 115-152 |
| C ₁₇ C ₁₈ | 10n | Min. Dipped Polyester | 115-051 |
| C ₁₉ C ₂₀ | 47n | Min. Dipped Polyester | 115-089 |
| C ₂₁ C ₂₂ | 470n | Min. Dipped Polyester | 115-130 |
| C ₂₃ C ₂₄ | 2n2 | Miniature Polyester | 112-721 |
| C ₂₅ C ₂₆ | 22n | Min. Dipped Polyester | 115-067 |

Determination of gain, bandwidth, attack and decay times

The mid band gain of the second stage, which is run in parallel feedback configuration, is determined by the ratio of the 10k internal feedback resistor and the 680R resistor in series with the output of the first stage. This gain may be reduced by wiring an external feedback resistor, R_{ext} , between pins 7 and 8. The gain will then be given by the expression:

$$G = \frac{R_{ext} \times 10,000}{(R_{ext} + 10,000) \times 680} \quad (R_{ext} \text{ in ohms})$$

The minimum permissible value for R_{ext} is 680R. The threshold point, i.e. the input level at which A.G.C. action commences, is approximately 1mV for $R_{ext} = \infty$ and approximately 8mV for $R_{ext} = 1k$.

The low frequency -3dB point is determined by the series combination of the internal 680R resistor and C_1 . The high frequency -3dB point is determined by the parallel combination of the internal 10k gain-setting resistor, any external resistor R_{ext} , and C_2 . Using the typical values $C_1 = 1\mu$, $C_2 = 4n7$, and $R_{ext} = \infty$, the -3dB points will occur at 234Hz and 3386Hz.

Normally the 6270 device is required to respond quickly by holding the output level almost constant as the input is increased. This "attack time", i.e. the time taken for the output to return to within 10% of the original level following a 20dB increase in the input level, will be approximately 20ms with the circuit in figure 11. It is determined by the value of C_T and can be calculated approximately by the formula:

$$\text{Attack time} \approx 0.4\text{ms}/\mu\text{F}$$

The decay time is determined by the discharge rate of the capacitor, this being dependent on the values of R_T and C_T . For $R_T = 1M$ and $C_T = 47\mu$ the decay time is approximately 20dB/second. Other values of R_T may be used to vary the decay time for specific applications.

Figure 10(a) Voltage gain (single ended input) - typical

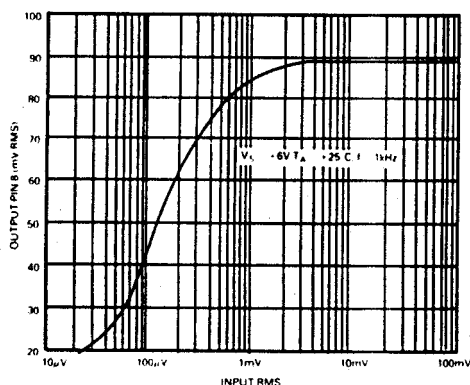
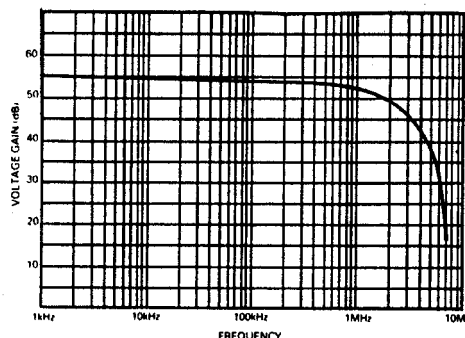


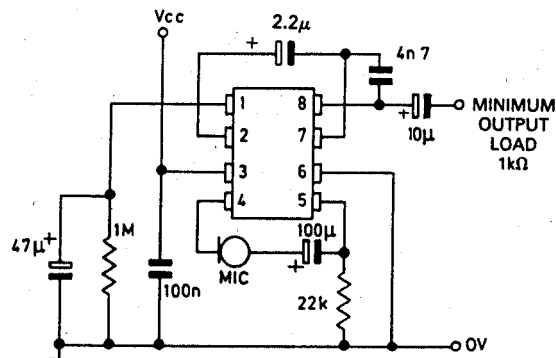
Figure 10(b) Open loop frequency response (typical)



Typical application

Figure 11 shows a typical application with the 6270 used as preamplifier for a 300Ω microphone. The bandwidth is approximately from 230Hz to 3,400Hz (-3dB). The input should normally be a.c. coupled, but if for any reason the coupling capacitor is omitted, the d.c. resistance between pins 4 and 5 should be less than 10 ohms. The 22k resistor

Figure 11



between pin 5 and ground is necessary to ensure that the offsets in the device at the onset of A.G.C. are of such polarity as to inhibit oscillation. If it is required to use the device with an unbalanced source, then the input may be A.C. coupled to pin 4 or pin 5, the unused input remaining floating. Any tendency to pick up noise when used in this mode may be inhibited by decoupling the unused input to ground by a 1000pF capacitor. **The inputs must not be D.C. grounded.**

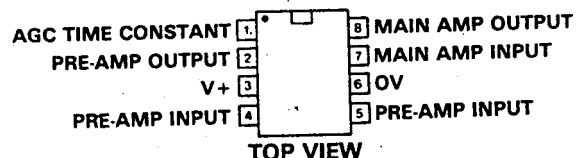
Bandwidth, gain, attack and decay times may be altered in accordance with the information given above to suit the differing requirements of specific applications.

6270

An integrated circuit combining the functions of audio amplifier and Voice Operated Gain Adjusting Device (V.O.G.A.D.), designed to accept signals from a low output microphone and to provide an essentially constant output signal of 90mV for a 60dB range of input. The dynamic range, attack and decay times are controlled by external components. Typical applications include audio A.G.C. systems, transmitter overmodulation protection, tape recorders, etc.

Absolute Maximum Ratings

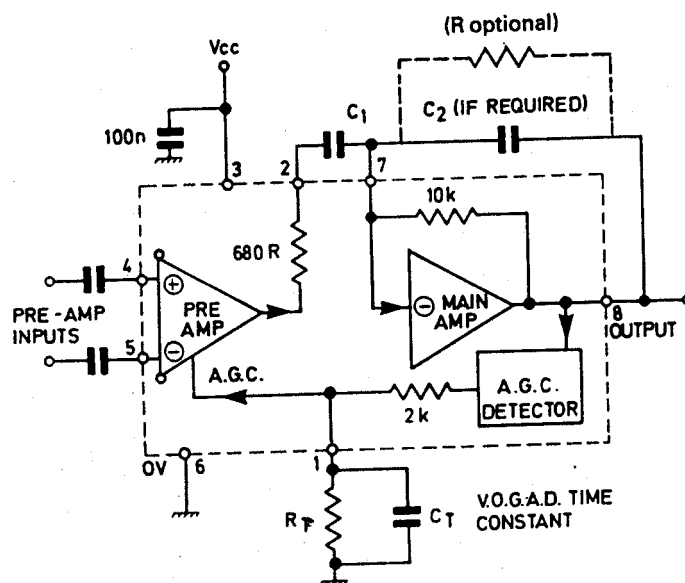
Supply voltage V_{CC} _____ +12V
Storage temperature range T_{stg} _____ -55 to +125°C



Electrical characteristics

| Parameter | Symbol | Test Conditions | min. | typ. | max. | units |
|------------------------------|-------------|------------------------------|------|------|------|----------|
| Supply voltage | V_{CC} | | 4.5 | 6 | 10 | V |
| Supply current | I_Q | | — | 5 | 10 | mA |
| Input impedance | $Z_{IN(S)}$ | Single ended, pin 4 or pin 5 | — | 150 | — | Ω |
| Differential input impedance | $Z_{IN(D)}$ | Input between pins 4 & 5 | — | 300 | — | Ω |
| Voltage gain | G_v | 72 μ V rms input pin 4 | 40 | 52 | — | dB |
| Output level | V_{OUT} | 4mV rms input pin 4 | 55 | 90 | 140 | mV rms |
| Total harmonic distortion | T.H.D. | 90mV input pin 4 | — | 2 | 5 | % |
| Operating temperature range | T_{AMB} | | -30 | | +85 | °C |

Figure 9



Circuit description

The principal elements of the device are shown in figure 9. The differential input preamplifier is A.G.C. controlled. The output from this stage is a.c. coupled via a capacitor to the second stage which is gain programmable by a single resistor to enable the overall sensitivity to be set. Adding a capacitor in parallel with this resistor permits the H.F.

response to be tailored, if required. The output from the second stage provides the main audio output from the device, and also drives the A.G.C. detector. The detected output, which is input level dependent, is applied to the time constant circuit and the A.G.C. controlled first stage. The second stage is run in inverting mode.

HA12017

A low noise, very low distortion pre-amplifier i.c. designed for high quality magnetic cartridge amplification using RIAA equalisation.

Absolute maximum ratings

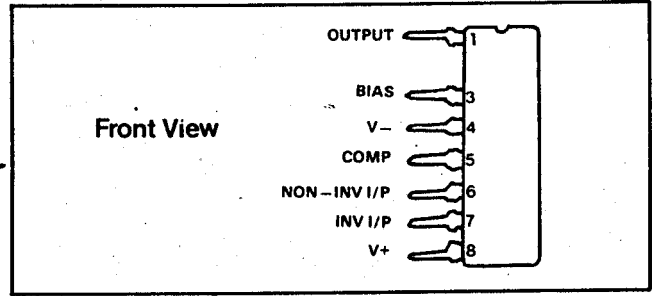
Supply voltage V_{CC} $\pm 26.5V$
 Power dissipation (T_A 25°C) P_T 500mW
 Storage temperature range T_{stg} -55 to +125°C

Electrical characteristics

($V_{CC} = \pm 24V, T_A = 25^\circ C$)

Recommended operating conditions

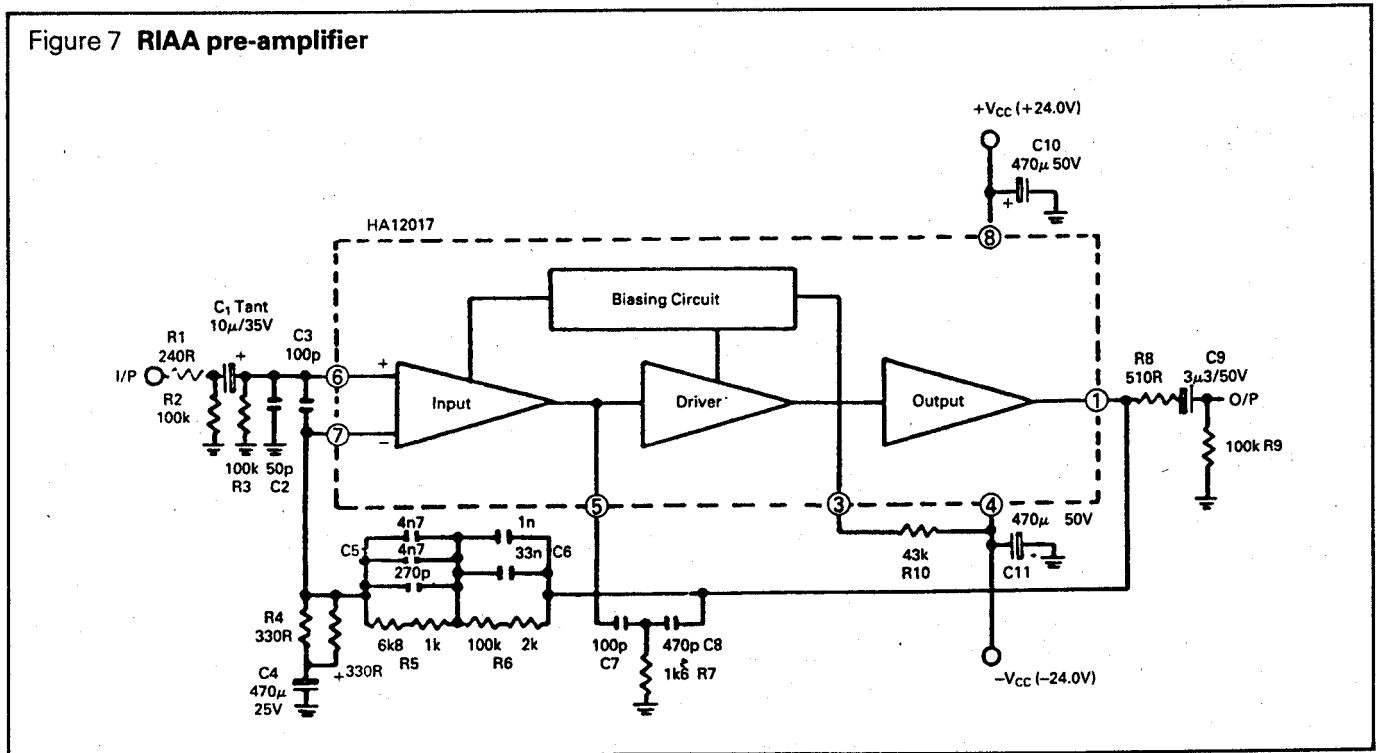
Power supply voltage V_{CC} $\pm 24V$
 Minimum power supply voltage $\pm 6V$
 Operating temperature range -30 to +75°C



| Parameter | Symbol | Test Conditions | min. | typ. | max. | unit |
|---------------------------|--------------|---------------------------------------|------|-------|------|---------|
| Quiescent Current | I_o | no input signal | | 4.0 | 6.0 | mA |
| Open Loop Voltage Gain | $G_{V(O.L)}$ | $f = 1kHz$ | 95 | 105 | - | dB |
| Total Harmonic Distortion | THD | $f = 1kHz, V_{out} = 10V$ | - | 0.002 | 0.01 | % |
| Output Voltage | V_{out} | $f = 1kHz, THD = 0.1\%$ | 13.5 | 14.7 | - | V |
| Overload Margin | - | $f = 1kHz, THD = 0.1\% G_v = 35.9dB$ | - | 235 | - | mV |
| Supply Ripple Rejection | SVR+ | $f = 100Hz R_g = 43\Omega$ | - | 56 | - | dB |
| | SVR- | $f = 100Hz R_g = 43\Omega$ | - | 45 | - | dB |
| Output Noise Voltage 1 | V_{n1} | $R_k = 43\Omega, IHF-A$ Network | - | 11.5 | 15.6 | μV |
| Output Noise Voltage 2 | V_{n2} | $R_k = 3.3k\Omega, BW -20Hz$ to 20kHz | - | 53 | 90 | μV |

NOTES: 1. All the parameters except $G_{V(O.L)}$ are tested with RIAA curve and $G_v = 35.9dB$. ($A_v = 62$).
 2. R_k = Source impedance to pin 6.

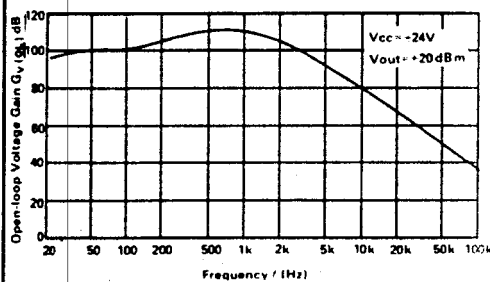
Figure 7 RIAA pre-amplifier



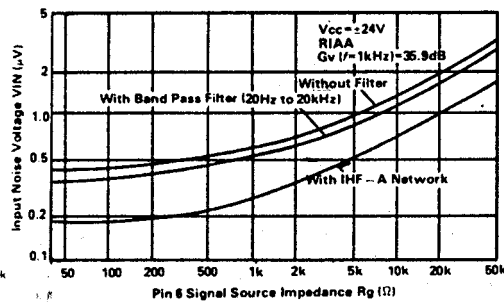
The RIAA pre-amplifier circuit is designed to accurately follow the RIAA playback curve, consequently some of the components in the feedback circuit consist of combinations of standard value capacitors and resistors in order to achieve an accurate response (e.g. 4n7 + 4n7 + 270p). For less deman-

ding applications standard preferred value components may be substituted in place of these networks. Input impedance of the amplifier circuit is approximately 50k Ω in order to match the load impedance requirements of the popular dynamic cartridges.

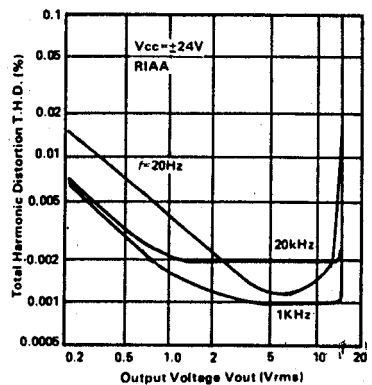
Figure 8
Open loop voltage gain V
frequency



Input noise voltage V
source impedance



THD V output voltage



RIAA Pre-amplifier external component functions

| Component | Recommended Value | Function |
|-----------|-------------------|---|
| R1 | 240Ω | Protects the i.c. from abnormal input voltage. Prevents parasitic oscillation caused by signal-source impedance. Decreases high-frequency disturbance. |
| R2 | 100kΩ | Passes the electric charge of C1. Decides Rin (input resistance) $R_{in} = R1 + (R2/R3)$ |
| R3 | 100kΩ | Supplies DC bias to pin-6 (input pin). Decides input resistance. |
| R4 | 165Ω | Decides voltage gain as feedback resistance. |
| R5 | 7.8kΩ | Decides RIAA characteristics, in pairs with C5 and C6. |
| R6 | 102kΩ | |
| R7 | 1.6kΩ | In a pair with C8, decides the frequency at which Gv (OL) characteristic changes from -12dB/oct to -6dB/oct. |
| R8 | 510Ω | Prevents parasitic oscillation caused by capacitive load. |
| R9 | 100kΩ | Keeps the voltage of output terminals at DC standard level. Prevents shock noise caused by function-switching. |
| R10 | 43kΩ | Decides basic bias current $R10 = (+V_{CC} - (-V_{CC}) - 5) k\Omega$ |
| C1 | 10uF | Input coupling. |
| C2 | 50pF | In combination with C3, increases stability of large-amplitude operation in high frequency range. |
| C3 | 100pF | In strong field, prevents detection of TV, FM and AM signals. |
| C4 | 470uF | Supplies full DC-feedback. Decides roll off frequency (f_L) in low frequency range. $f_L = 3Hz$ (Typical application) $f_L = \frac{1}{2\pi C4.R4}$ |
| C5 | 9670pF | Decides RIAA characteristics in pairs with R5 and R6. |
| C6 | 34000pF | |
| C7 | 100pF | Supplies phase-compensation. |
| C8 | 470pF | In a pair with R7, decides the frequency at which Gv (OL) characteristic changes from -12dB/oct to -6dB/oct. |
| C9 | 3.3uF | Output-coupling. |
| C10 | 470uF | Removes ripple on Vcc line. |
| C11 | 470uF | |